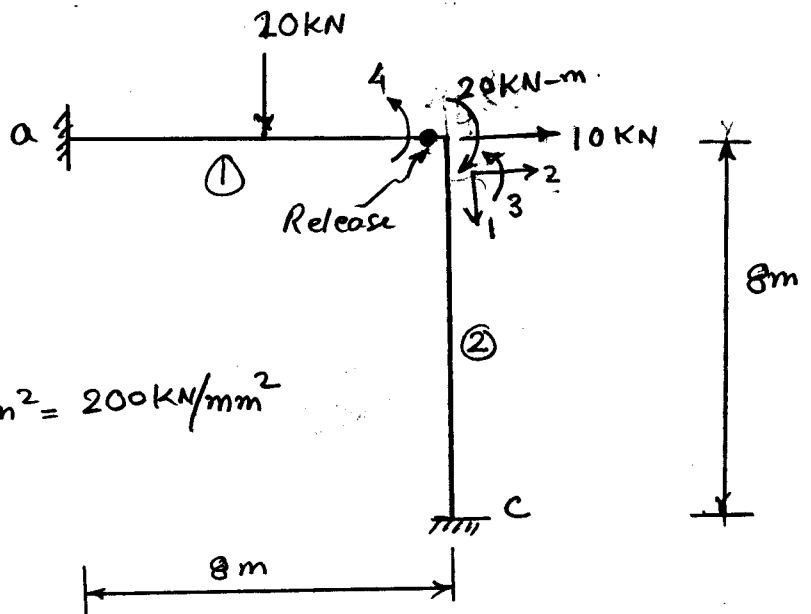
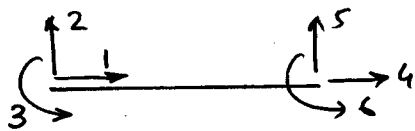


Example Problem

Analyze the Frame shown below in which member ab has a moment release at end b



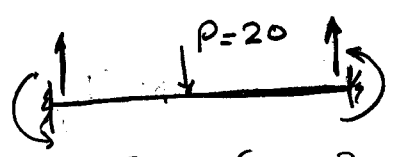
$$\begin{aligned}
 A &= 6000 \text{ mm}^2 \\
 I &= 200 \times 10^6 \text{ mm}^4 \\
 E &= 200,000 \text{ N/mm}^2 = 200 \text{ kN/mm}^2
 \end{aligned}$$



$$\begin{Bmatrix} F_1 \\ F_2 \\ M_3 \\ F_4 \\ F_5 \\ M_6 \end{Bmatrix} = E \begin{bmatrix} A/L & 0 & 0 & -A/L & 0 & 0 \\ 0 & \frac{12I}{L^3} & \frac{6I}{L^2} & 0 & -\frac{12I}{L^3} & \frac{6I}{L^2} \\ 0 & \frac{6I}{L^2} & \frac{4I}{L} & 0 & -\frac{6I}{L^2} & \frac{2I}{L} \\ -A/L & 0 & 0 & A/L & 0 & 0 \\ 0 & -\frac{12I}{L^3} & -\frac{6I}{L^2} & 0 & \frac{12I}{L^3} & -\frac{6I}{L^2} \\ 0 & \frac{6I}{L^2} & \frac{2I}{L} & 0 & -\frac{6I}{L^2} & \frac{4I}{L} \end{bmatrix} \begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \\ \Delta_4 \\ \Delta_5 \\ \Delta_6 \end{Bmatrix}$$

Example Problem

$$K_{G0} = \begin{bmatrix} & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ 200 & & & & \end{bmatrix} \begin{matrix} 1 & 2 & 4 \\ \hline \\ \\ \\ \end{matrix} \quad D_{A0} = \begin{Bmatrix} 6 \\ 6 \\ 0 \\ \hline 1 \\ 2 \\ 4 \end{Bmatrix}$$



$$FEM = \begin{Bmatrix} 0 \\ P/2 \\ PL/8 \\ \hline 0 \\ P/2 \\ -PL/8 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 10 \\ 20 \\ \hline 0 \\ 10 \\ -20 \end{Bmatrix} \begin{matrix} \\ \\ \\ \\ \text{KN} \\ \text{KN-m} \end{matrix}$$

$$= \begin{Bmatrix} 0 \\ 10 \\ 20,000 \\ \hline 0 \\ 10 \\ -20,000 \end{Bmatrix} \begin{matrix} \\ \text{KN-mm} \\ \\ \text{KN} \\ \text{KN-mm} \end{matrix}$$

$$F_{EQ} = -FEM = \begin{Bmatrix} 0 \\ -10 \\ -20,000 \\ \hline 0 \\ -10 \\ -20,000 \end{Bmatrix}$$

$$F_{EQ \text{ Global}} = [T]^T \{F_{EQ}\}$$

$$= \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} 0 \\ -10 \\ 20,000 \end{Bmatrix} = \begin{Bmatrix} 10 \\ 0 \\ 20,000 \end{Bmatrix}$$

$$\Rightarrow F_{EQ \text{ Global}} = \begin{Bmatrix} \hline \hline \hline \hline 10 \\ 0 \\ 20,000 \end{Bmatrix} \quad D_{A1} = \begin{Bmatrix} 0 \\ 6 \\ 0 \\ \hline 1 \\ 2 \\ 4 \end{Bmatrix}$$

Example Problem

Member 2

$$K_{(2) \text{ local}} = K_{\text{Global}} = 200$$

$$\begin{bmatrix} 0.75 & 0 & 0 \\ 0 & 0.00469 & 18.75 \\ 0 & 18.75 & 100,000 \end{bmatrix} \begin{matrix} \\ \\ \hline \end{matrix} \begin{matrix} 1 \\ 2 \\ 3 \\ \hline 0 \\ 0 \\ 0 \end{matrix}$$

Structural Stiffness Matrix

$$K_G = \begin{matrix} 200 \\ \begin{bmatrix} 1 & 2 & 3 & 4 \\ 0.00469 + 0.75 & 0 & 0 & 18.75 \\ 0 & 0.75 + 0.00469 & 18.75 & 0 \\ 0 & 0 + 18.75 & 100,000 & 0 \\ 18.75 & 100 & 0 & 100,000 \end{bmatrix} \end{matrix}$$

$$K_G = \begin{matrix} 200 \\ \begin{bmatrix} 0.75469 & 0 & 0 & 18.75 \\ 0 & 0.75469 & 18.75 & 0 \\ 0 & 18.75 & 100,000 & 0 \\ 18.75 & 0 & 0 & 100,000 \end{bmatrix} \end{matrix}$$

$$F_{EQ} = \begin{matrix} \text{Global} \\ \begin{bmatrix} 10 + \\ 0 + 10 \\ 0 - 20,000 \\ 20,000 \end{bmatrix} \end{matrix} = \begin{matrix} \begin{bmatrix} 10 \\ 10 \\ -20,000 \\ 20,000 \end{bmatrix} \\ \text{KN} \\ \text{KN} \\ \text{KN-mm} \\ \text{KN-mm} \end{matrix}$$

Example Problem

$$[K_G] \{\Delta\} = \{P_{EQ}\}$$

$$200 \begin{bmatrix} 0.75469 & 0 & 0 & 18.75 \\ 0 & 0.75469 & 18.75 & 0 \\ 0 & 18.75 & 100,000 & 0 \\ 18.75 & 0 & 0 & 100,000 \end{bmatrix} \begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \theta_3 \\ \theta_4 \end{Bmatrix} = \begin{Bmatrix} 10 \\ 10 \\ -20,000 \\ 20,000 \end{Bmatrix}$$

Direct Soln gives

$$\begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \theta_3 \\ \theta_4 \end{Bmatrix} = \frac{1}{200} \begin{Bmatrix} 8.3203 \\ 18.30467 \\ -0.203432 \\ 0.1984 \end{Bmatrix} = \begin{Bmatrix} 0.416 \\ 0.0915 \\ -0.001017 \\ 0.00099 \end{Bmatrix} \begin{matrix} \text{mm} \\ \text{mm} \\ \text{rad} \\ \text{rad} \end{matrix}$$

Alternately Condense out θ_4
From Global Equations

$$\begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{Bmatrix} \Delta_r \\ \Delta_c \end{Bmatrix} = \begin{Bmatrix} P_r \\ P_c \end{Bmatrix}$$

$$K_{21} \Delta_r + K_{22} \Delta_c = P_c$$

$$\Rightarrow \Delta_c = K_{22}^{-1} (P_c - K_{21} \Delta_r)$$

$$K_{11} \Delta_r + K_{12} \Delta_c = P_r$$

$$K_{11} \Delta_r + K_{12} (K_{22}^{-1} (P_c - K_{21} \Delta_r)) = P_r$$

$$\boxed{[K_{11} - K_{12} K_{22}^{-1} K_{21}] \Delta_r = P_r - K_{12} K_{22}^{-1} P_c}$$

Condensed Equations

Example Problem

$$K_{12} K_{22}^{-1} = 200 \begin{Bmatrix} 18.75 \\ 0 \\ 0 \end{Bmatrix} \times \left[\frac{1}{200 \times 100,000} \right]$$

$$= \frac{1}{100,000} \begin{Bmatrix} 18.75 \\ 0 \\ 0 \end{Bmatrix}$$

$$K_{12} K_{22}^{-1} K_{21} = \frac{200}{100,000} \begin{Bmatrix} 18.75 \\ 0 \\ 0 \end{Bmatrix} \begin{bmatrix} 18.75 & 0 & 0 \end{bmatrix}$$

$$= \frac{200}{100,000} \begin{bmatrix} 351.563 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$[\tilde{K}] = K_{11} - K_{12} K_{22}^{-1} K_{21}$$

$$[\tilde{K}] = 200 \begin{bmatrix} 0.75117 & 0 & 0 \\ 0 & 0.75469 & 18.75 \\ 0 & 18.75 & 100,000 \end{bmatrix}$$

$$[\tilde{P}] = P_W - K_{12} K_{22}^{-1} P_C$$

$$= \begin{Bmatrix} 10 \\ 10 \\ -20,000 \end{Bmatrix} - \frac{1}{100,000} \begin{Bmatrix} 18.75 \\ 0 \\ 0 \end{Bmatrix} \begin{bmatrix} 20,000 \end{bmatrix} = \begin{Bmatrix} 6.25 \\ 10 \\ -20,000 \end{Bmatrix}$$

Example Problem

$$[\tilde{K}] \{\Delta_r\} = \{P_r\}$$

$$\Rightarrow \{\Delta_r\} = [\tilde{K}]^{-1} \{P_r\}$$

$$\Rightarrow \{\Delta_r\} = \begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \theta_3 \end{Bmatrix} = \frac{1}{200} \begin{Bmatrix} 8.3204 \\ 18.304 \\ -0.2034 \end{Bmatrix} = \begin{Bmatrix} 0.0416 \\ 0.0915 \\ -0.001017 \end{Bmatrix}$$

Recovering the Condensed DOF

$$\Delta_c = \theta_4 = k_{22}^{-1} (P_c - k_{21} \Delta_r)$$

$$= \frac{1}{200 \times 100,000} \left[[20,000] - \frac{200}{200} [18.75 \ 0 \ 0] \begin{Bmatrix} 8.3204 \\ 18.304 \\ -0.2034 \end{Bmatrix} \right]$$

$$\Delta_c = \theta_4 = \frac{1}{200 \times 100,000} [19843.99] = \frac{1}{200} \times 0.1984 = 0.00099 \text{ rad.}$$

Hence the Complete Displacement Vector is again

$\begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \theta_3 \\ \theta_4 \end{Bmatrix} = \frac{1}{200} \begin{Bmatrix} 8.303 \\ 18.30467 \\ -0.203432 \\ 0.1984 \end{Bmatrix} = \begin{Bmatrix} 0.0416 \\ 0.0915 \\ -0.001017 \\ 0.00099 \end{Bmatrix}$	$\begin{matrix} \text{mm} \\ \text{mm} \\ \text{rad} \\ \text{rad} \end{matrix}$
--	--

Example Problem

As a Second Alternate we can condense out θ_4 at Element Level when processing Element ①

Recall that For Element ① we have the Equilibrium Equations in Global Coordinates as:

$$200 \begin{bmatrix} 0.00469 & 0 & | & 18.75 \\ 0 & 0.75 & | & 0 \\ \hline 18.75 & 0 & | & 100,000 \end{bmatrix} \begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \theta_4 \end{Bmatrix} = \begin{Bmatrix} 10 \\ 0 \\ 20,000 \end{Bmatrix}$$

$K_{G \text{ ①}}$ $F_{EQ G \text{ ①}}$

Condense out θ_4

$$K_{12} K_{22}^{-1} = 200 \begin{bmatrix} 18.75 \\ 0 \end{bmatrix} \left[\frac{1}{200 \times 100,000} \right] = 200 \begin{bmatrix} 9.375 \times 10^{-7} \\ 0 \end{bmatrix}$$

$$K_{12} K_{22}^{-1} K_{21} = 200 \begin{bmatrix} 9.375 \times 10^{-7} \\ 0 \end{bmatrix} \begin{bmatrix} 18.75 & | & 0 \end{bmatrix}$$

$$K_{12} K_{22}^{-1} K_{21} = 200 \begin{bmatrix} 1.7578 \times 10^{-5} & 0 \\ 0 & 0 \end{bmatrix}$$

$$\tilde{K}_{G \text{ ①}} = K_{11} - K_{12} K_{22}^{-1} K_{21}$$

$$\tilde{K}_{G \text{ ①}} = 200 \begin{bmatrix} 0.00469 & 0 \\ 0 & 0.75 \end{bmatrix} - 200 \begin{bmatrix} 1.7578 \times 10^{-5} & 0 \\ 0 & 0 \end{bmatrix}$$

$$\tilde{K}_{G \text{ ①}} = 200 \begin{bmatrix} 0.004672 & 0 \\ 0 & 0.75 \end{bmatrix} \quad \tilde{D}_{A \text{ ①}} = \begin{Bmatrix} 1 \\ 2 \end{Bmatrix}$$

Example Problem

$$\tilde{P}_{G①} = P_w - k_{12} k_{22}^{-1} P_c$$

$$= \begin{Bmatrix} 10 \\ 0 \end{Bmatrix} - 200 \begin{bmatrix} 9.375 \times 10^{-7} \\ 0 \end{bmatrix} [20,000]$$

$$\tilde{P}_{G①} = \begin{Bmatrix} 6.25 \\ 0 \end{Bmatrix}$$

$$\tilde{D}_{A①} = \begin{Bmatrix} 1 \\ 2 \end{Bmatrix}$$

Assembled Structure Stiffness Matrix

$$\tilde{K}_G = 200 \begin{bmatrix} 1 & 2 & 3 \\ 0.004672 & 0 & 0 \\ +0.75 & 0.75 & 0 \\ 0 & +0.00469 & +18.75 \\ 0 & +18.75 & +100,000 \end{bmatrix}$$

$$\tilde{K}_G = 200 \begin{bmatrix} 0.754672 & 0 & 0 \\ 0 & 0.754672 & 18.75 \\ 0 & 18.75 & 100,000 \end{bmatrix}$$

$$\tilde{P}_{EQ} = \begin{Bmatrix} 6.25 + 0 \\ 0 + 10 \\ 0 - 20,000 \end{Bmatrix} = \begin{Bmatrix} 6.25 \\ 10 \\ -20,000 \end{Bmatrix}$$

$$\tilde{K}_G \tilde{\Delta}_r = \tilde{P}_{EQ}$$

$$\Rightarrow \tilde{\Delta}_r = \tilde{K}_G^{-1} P_{EQ}$$

$$\Rightarrow \tilde{\Delta}_r = \begin{Bmatrix} \Delta_1 \\ \Delta_2 \\ \Delta_3 \end{Bmatrix} = \frac{1}{200} \begin{Bmatrix} 8.2817 \\ 18.305 \\ -0.2034 \end{Bmatrix}$$

$$= \begin{Bmatrix} 0.416 \\ 0.0915 \\ -0.001017 \end{Bmatrix} \begin{matrix} \text{mm} \\ \text{mm} \\ \text{rad} \end{matrix}$$

Same as before

Example Problem

Hence, we have demonstrated that we can provide a force release in the following number of manners:

- Introduce an extra Degree of freedom and solving directly
- Assemble Global Structure Equilibrium Equations and Condense out the Degree of Freedom corresponding to the Released Force
- Condense out the Degree of Freedom corresponding to Released Force at Element Formulation Level and then proceed with Stiffness Assembly

Determination of Member Forces

$$\{F\} = [K]\{\Delta\} + FEM.$$

① Fixed End Member

$$= \frac{200}{200} \begin{bmatrix} 0 & 0 & 0 \\ -0.75 & 0 & 0 \\ 0 & -0.00469 & 18.75 \\ 0 & -18.75 & 50,000 \end{bmatrix} \begin{Bmatrix} -8.303 \\ 18.30467 \\ 0.1984 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 10 \\ 20,000 \end{Bmatrix}$$

$$= \begin{Bmatrix} +6.227 \\ +3.634 \\ +9576.8 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 10 \\ 20,000 \end{Bmatrix} = \begin{Bmatrix} 6.227 \\ 13.634 \\ 29576.8 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-mm} \end{matrix} = \begin{Bmatrix} 6.23 \\ 13.63 \\ 29.58 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-m} \end{matrix}$$

② Hinged End Member

$$= \frac{200}{200} \begin{bmatrix} 0.75 & 0 & 0 \\ 0 & 0.00469 & -18.75 \\ 0 & -18.75 & 100,000 \end{bmatrix} \begin{Bmatrix} -8.303 \\ 18.30467 \\ 0.1984 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 10 \\ -20,000 \end{Bmatrix}$$

$$= \begin{Bmatrix} -6.227 \\ -3.634 \\ +19496.8 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 10 \\ -20,000 \end{Bmatrix} = \begin{Bmatrix} -6.227 \\ +6.366 \\ -503 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-mm} \end{matrix} = \begin{Bmatrix} -6.227 \\ +6.366 \\ -0.5 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-m} \end{matrix}$$

Example Problem

Forces in Member ②

Top End

$$\frac{200}{200} \begin{bmatrix} 0.75 & 0 & 0 \\ 0 & 0.00469 & 18.75 \\ 0 & 18.75 & 100,000 \end{bmatrix} \begin{Bmatrix} 8.3203 \\ 18.30467 \\ -0.1984 \end{Bmatrix} = \begin{Bmatrix} 6.24 \\ -3.63 \\ -19.496 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-mm} \end{matrix}$$

$$= \begin{Bmatrix} 6.24 \\ -3.63 \\ -19.5 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-m} \end{matrix}$$

Bottom End

$$\frac{200}{200} \begin{bmatrix} -0.75 & 0 & 0 \\ 0 & -0.00469 & -18.75 \\ 0 & 18.75 & 50,000 \end{bmatrix} \begin{Bmatrix} 8.3203 \\ 18.30467 \\ -0.1984 \end{Bmatrix} = \begin{Bmatrix} -6.24 \\ +3.63 \\ -9.567 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-mm} \end{matrix}$$

$$= \begin{Bmatrix} -6.24 \\ +3.63 \\ -9.576 \end{Bmatrix} \begin{matrix} \text{KN} \\ \text{KN} \\ \text{KN-m} \end{matrix}$$

